

# VECTOR MEASURING WITH 7-STATE PERTURBATION TWO PORTS

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**Abstract:** A novel construction of a 7-state perturbation two-port vector network analyzer is presented. It consists of 7 basic passive two-port discontinuities, which enable a simple realization with good electrical parameters in certain parts of Smith chart. The new approach makes it possible to choose the best states for any specific area in Smith Chart. Mathematical backgrounds of the approach, as well as new test criteria are designed.

## Introduction

Vector network analyzers (VNA) based on frequency conversions are widely used for wideband vector measurements. They are complex and costly systems. On the other hand, scalar network analyzers (SA) are simpler and cheaper, but they only give scalar information. A concept for vector measurement based on SA and perturbation two-port (PTP) was presented in [1]. In this paper, a significant improvement of the original concept based on 7-state perturbation two-port is presented. A typical arrangement of the new PTP vector network analyzer with seven switched discontinuities is presented in Fig.1.

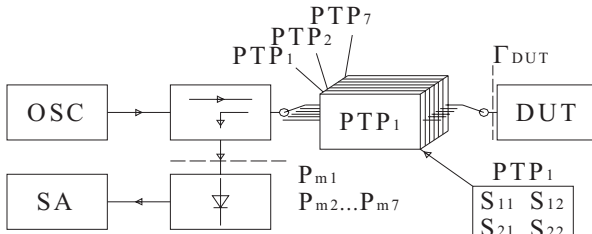


Fig. 1: Measuring system with SA and 7-state perturbation two-port

## Theory

The main idea of vector measuring with a scalar analyzer and PTPs is derived from the relation (1) between  $\Gamma_{DUT}$  and  $P_m$ , where  $P_m$  is the measured reflection power and  $\Gamma_{DUT}$  is the reflection coefficient of the device under test (DUT). This relation could be modified to the quadratic plane equation where  $A_x, B_x, \dots, G_x$  are real coefficients. The quadratic plane given by (2) is completely defined at one frequency by these seven real constants. The constants can be found by calibration [2].

$$P_m = |\Gamma_m|^2 = \left| S_{11} + \frac{S_{21} \cdot S_{12} \cdot \Gamma_{DUT}}{1 - S_{22} \cdot \Gamma_{DUT}} \right|^2 \quad (1)$$

(2)

$$A_x |\Gamma_{DUT}|^2 + B_x \Re(\Gamma_{DUT}) + C_x \Im(\Gamma_{DUT}) + D_x P_m \Re(\Gamma_{DUT}) + E_x P_m \Im(\Gamma_{DUT}) + F_x P_m |\Gamma_{DUT}|^2 + G_x + P_m = 0$$

For example, if we have the 3-state PTP with optimally spaced quadratic plane, and one DUT with reflection coefficient  $\Gamma_{DUT} = 0.3 + 0.8j$ , we get three measured reflection power  $P_m$ . Primary value  $\Gamma_{DUT}$  is given as a solution of three linear equations, where  $P_m$  and  $A_x, B_x, \dots, G_x$  are required. The graphic representation is described at Fig.2 where the vertical line with diamonds determines the  $\Gamma_{DUT}$  position.

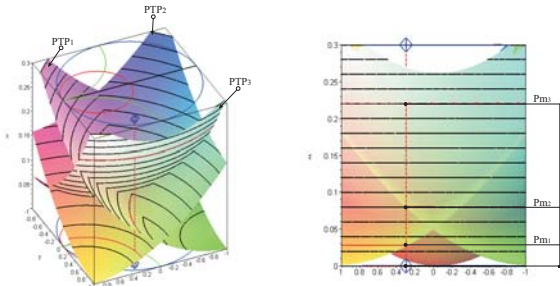


Fig. 2: Measuring with 3-state optimally spaced PTP quadratic planes

## 7-State PTP

Because 3-state PTPs with optimally oriented frequency independent quadratic planes are difficult to construct, the novel 7-state PTP consists of elementary two ports discontinuities, which were simulated and measured. Typical quadratic planes are shown at Fig.3.

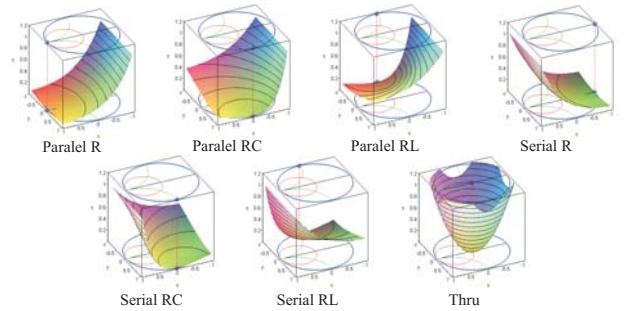


Fig. 3 Examples of 7-state PTP quadratic planes

## Test criteria

Now we have 7-state PTP system where only three states for  $\Gamma_{DUT}$  determination are needed. The question is to find out how to choose the three best quadratic planes, which produce the lowest measuring error in a specific area of Smith Chart. Three basic test criteria can then be used.

**The gradient criterion:** If a state of the PTP has lower gradient at a specific area, even a small error in the measured reflected power  $P_m$  will produce significant error during  $\Gamma_{DUT}$  determination. Fig.4 shows an example of this criterion.

**The angle criterion:** Two quadratic planes can be considered for any given  $\Gamma_{DUT}$ . It is possible to construct a vertical line perpendicular to the x-y plane where the  $\Gamma_{DUT}$  is localized. The distance between the x-y plane and quadratic plane cross point is equal to the measured reflected power  $P_m$ , see Fig.2. Then the reverse task is solved during measurement. For two quadratic planes we have two measured  $P_m$  that define a set of  $\Gamma_{DUT}$ . These two sets are represented as two circles which have two cross points. One is at the  $\Gamma_{DUT}$  position and the second is a mirror. This criterion is then to find the circle cross angle for the whole x-y plane. Angles between 30-90 degrees are acceptable, producing low errors in  $\Gamma_{DUT}$  determination process, see Fig.4.

**The vector product test:** This is a more complex criterion. For two quadratic planes, we can define two gradient vectors in each point of the x-y plane. The module of the vector product of the gradient vectors displayed at the x-y plane gives information about both gradient and angle results.

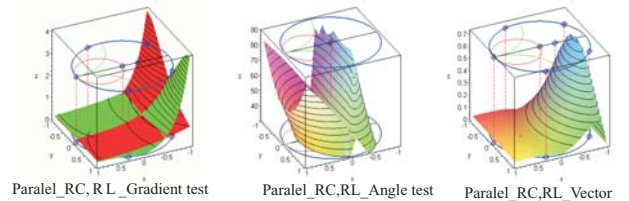


Fig. 4: Three basic criteria for one pair of quadratic planes

**The error power test:** In real measurements some noise error signal superimposed on measured power must be considered. This noise will produce error during the  $\Gamma_{DUT}$  space determination. Oscillating circles which determine the  $\Gamma_{DUT}$  position will provide the error area with four border cross points. When the geometric distance between the  $\Gamma_{DUT}$  position and the most outlying point is computed and displayed in the x-y plane, it is

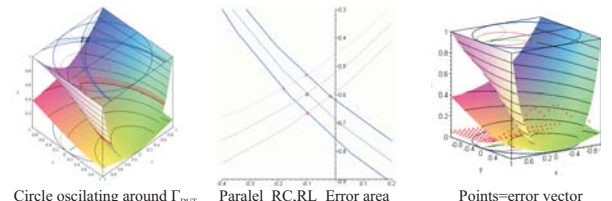


Fig. 5 Error power test

## Conclusion

A new concept for vector measurement based on scalar network analyzer and 7-state PTPs was designed. New test criteria for 7-state to 3-state PTP reduction were developed and verified by computer simulations. This approach allows a simple realization of individual states of the PTP and low measurement uncertainties.